

# PRODUCTION OF BATTERY GRADE NICKEL AND COBALT SULFATE FROM NICKEL LATERITE ORE

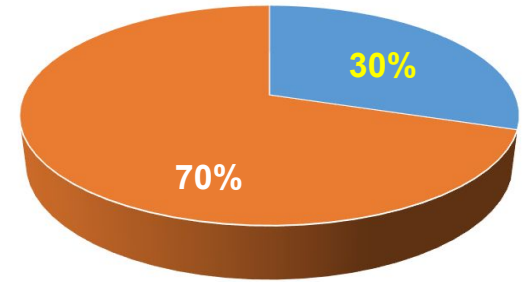
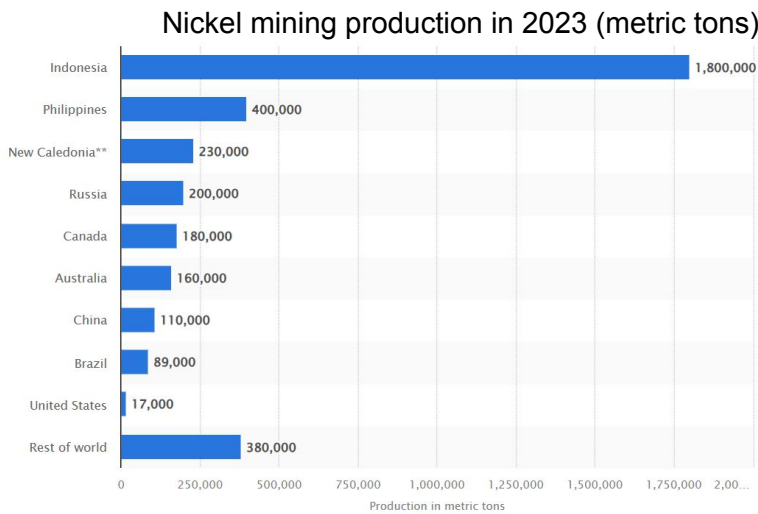
**Kaixi Jiang\*, Haibei Wang, Sanping Liu**  
**BGRIMM / Zijin Ming Group / Fuzhou University**

**May 28<sup>th</sup>, 2024 Perth, Australia**

\*Presenter

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- 1. Introduction**
- 2. Leaching of Nickel Laterite Ores**
- 3. MHP Refining**
- 4. Summary**



■ Nickel sulfide ore ■ Nickel laterite ore

Proportion of ore types in nickel production

- World nickel production: 3.57 Mt in 2023.
- Indonesia nickel production: 1.8 Mt in 2023, accounting for 50.4% of world production.
- Proportion of ore types in nickel production: 30% sulfide ore VS 70% laterite ore.

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## ◆ Main processes Nickel laterite ores

### Pyrometallurgy

**RKEF → ferronickel (Ni>25%)**

**Blast furnace → pig iron (Ni>5%)**

**Matte smelting → nickel matte (Ni~70%)**

**Rotary kiln reduction -- magnetic separation → metallic Ni/Fe powder**

#### Characteristics

- mature and widely used
- high Ni recovery
- high energy consumption
- poor adaptability, suitable for processing high-grade laterite ore
- Co in ferronickel / pig iron devaluated

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## ◆ Main processes Nickel laterite ores

### Hydrometallurgy

**High pressure acid leaching (HPAL):** a standard technology for limonite laterite ores.

- High nickel extraction ( $E_{Ni} > 95\%$ ) ;
- Low acid consumption (iron precipitated as hematite);
- High pressure up to 5.5MPa, high temp. up to 270°C.

#### Alternative

**Atmosphere tank leaching (ATL):** LOGIC: Recovery exchanges costs.

Primary leaching: high acid concentration, high Ni and Fe extraction;

Secondary leaching: feed - high magnesium laterite (saprolite), neutralization and iron precipitation with saprolite leaching.

- Low CAPEX and OPEX;
- Lower nickel extraction ( $E_{Ni}$  85~93%) ;
- Higher acid consumption ( up to 90% iron precipitated as jarosite or goethite, maybe with lime addition).

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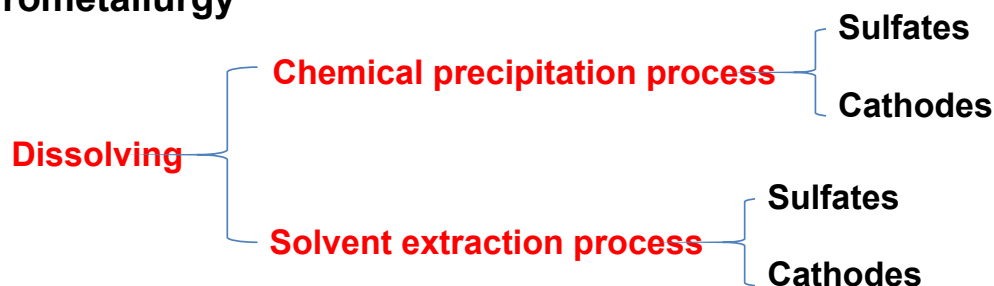
## ◆ Main processes MHP refining

### Pyrometallurgy

Precious nickel matte → refining products

Reduction anode → cathode

### Hydrometallurgy



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### ◆ Inverse Leaching\* Process

(\*ALTA 2013 keynote)

2 types of laterite ores



↑  
Limonite (high Fe, low Mg)

↑  
Saprolite (low Fe, high Mg)

#### General process

- Limonite ore → HPAL
- Saprolite ore → AL (Neutralization + Leaching)

#### Inverse leaching process

- Limonite ore → AL (High acid, ~95 °C)
- Saprolite ore → PAL (150~160°C)

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### ◆ Inverse Leaching Process

#### BGRIMM's special flowsheet — an inverse leaching process (patented)

##### Primary leaching: atmosphere tank leaching

- Feed: limonite portion of laterite ores;
- ~95 °C, input: 100% acid, 97~99%  $E_{Ni}$  &  $E_{Fe}$ ;

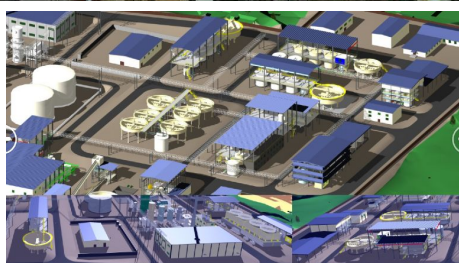
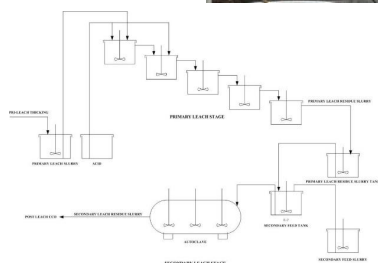
##### Secondary leaching: autoclave leaching

- Feed: saprolite portion of laterite ores;
- Around 150~160°C, no acid input, 500~600kPa;
- Total  $E_{Ni}$  93~96%;
- No acid consumption for 90~95% Fe.

**The leaching combination changes the BIG DIFFICULTY of HPAL to “a common routine process”!**

### ◆ Inverse Leaching Process

Pilot plant photos



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### ◆ Inverse Leaching Process

Leaching performance of IL process

	Primary Leach Results			Secondary Leach Results		
	Ni	Fe	Mg	Ni	Fe	Mg
Residue Solids Grade (%)	0.05	8.38	1.32	0.15	21.11	1.57
PLS Concentration (g/L)	5.08	56.70	40.11	5.29	3.40	49.41
Solids-based Metal Extraction (%)	98.40	80.63	94.56	93.44	19.94	92.65
Residue Free Acid (g/L)	18.85	(H <sub>2</sub> SO <sub>4</sub> )		15.39	(H <sub>2</sub> SO <sub>4</sub> )	
% Mass Remaining (%)	48.10			64.37		

### ◆ Two-stage Pressure Leaching Process

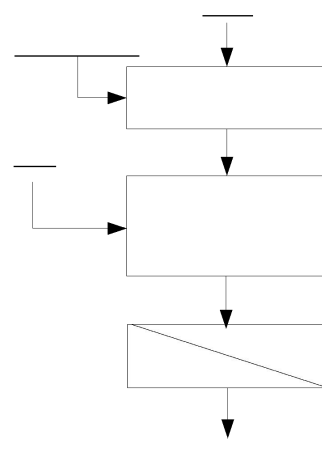
#### HPAL — AL process used in Indonesia

##### ◆ Limonite ore → HPAL

- Ni and Co extraction > 95%
- Fe precipitation → acid release

##### ◆ Saprolite ore → AL

- HPAL leached slurry is neutralized by SAP to reduce acid consumption
- Ni extraction : 40~60% (low)



HPAL — AL process

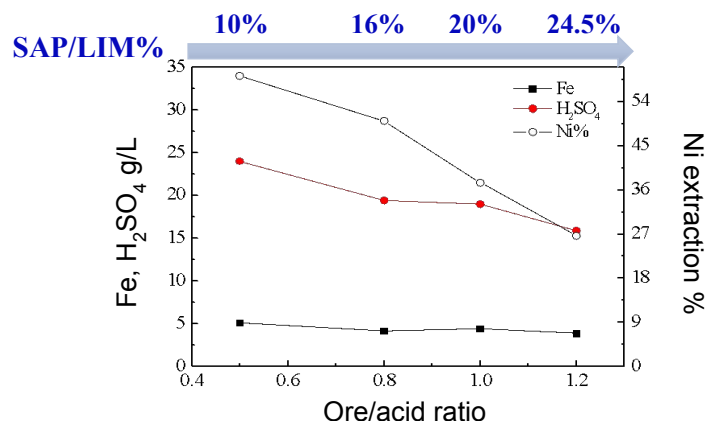
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### ◆ Two-stage Pressure Leaching Process

#### HPAL — AL process used in Indonesia

##### ◆ Disadvantages

- Ni extraction in AL : 50%.
- More Fe is leached when Ni extraction reaches 65~70% with acid introduction.



$C_{Fe}$  comparison of HAPL and AL PLS with different SAP additions (AL remaining acid 10g/L)

SAP/LIM%	Fe, g/L	
	HPAL solution	AL solution
8	2.8	4.2
20	1.6	6.2

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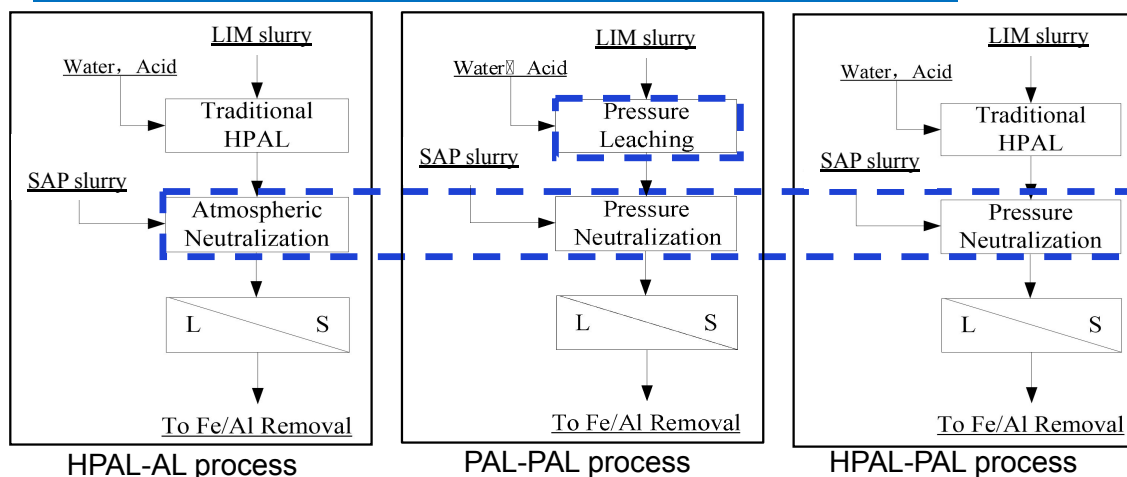
### ◆ Two-stage Pressure Leaching Process

In order to improve the inverse leaching process and HPAL – AL process, BGRIMM proposed the combinations of two-stage leaching:

- AL – PAL (95 °C / 150~225 °C, 0.5~2.5 MPa)
- PAL – PAL (150~225 °C, 0.5~2.5 MPa)
- HPAL – PAL (240~270 °C, 3.3~5.5 MPa / 150~225 °C, 0.5~2.5 MPa)

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### ◆ Two-stage Pressure Leaching Process



Patented



### Two-stage pressure leaching process (PAL-PAL, HPAL-PAL)

- LIM → HPAL
- SAP → PAL: HPAL slurry flows to 2<sup>nd</sup> autoclave without flashing. SAP slurry is leached by using the heat and remaining acid of HPAL slurry.

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### ◆ Comparison of 3 leaching combinations

#### Leaching conditions:

- ◆ HPAL(250°C) –AL(95°C)
- ◆ HPAL(250°C) – PAL (230°C)
- ◆ PAL(225°C) -PAL(200°C)

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### ◆ Comparison 1:

#### HPAL(250°C) — AL(95°C)

- ◆ HPAL: Ni extraction >97%. AL: Ni extraction 47-56%
- ◆ Total Ni extraction ~85%.

LIM/SAP		100:25		100:30		100:35	
Leaching stage		HPAL	AL	HPAL	AL	HPAL	AL
Total extraction /%	Ni	96.91	86.80	97.58	85.93	97.58	82.63
Extraction in this stage/%	Ni	96.91	56.06	97.58	55.55	97.58	47.01

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### ◆ Comparison 2:

#### HPAL(250°C) — PAL (230°C)

- ◆ HPAL: Ni extraction >97%. PAL: Ni extraction 80-87.3%.
- ◆ Total Ni extraction 92-94%.

LIM/SAP		100:25		100:30		100:35	
Leaching stage		HPAL	PAL	HPAL	PAL	HPAL	PAL
Total extraction /%	Ni	97.73	94.10	97.91	93.45	96.74	92.15
Extraction in this stage/%	Ni	97.73	87.34	97.91	83.84	96.74	80.18

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### ◆ Comparison 3:

#### PAL(225°C) — PAL(200°C)

- ◆ PAL: Ni extraction >97%. PAL: Ni extraction 73-78.6%.
- ◆ Total Ni extraction 87.6-90.6%.

LIM/SAP		100:25		100:30		100:35	
Leaching stage		1	2	1	2	1	2
Total extraction /%	Ni	96.11	90.57	96.91	89.47	93.25	87.64
Extraction in this stage/%	Ni	96.11	78.63	96.91	75.64	93.25	73.00

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### ◆ Comparison of 3 leaching combinations

- ◆ Use heat and remaining acid of HPAL slurry, Ni extraction greatly improved.

SAP  $E_{Ni}$  56% (AL)→87% (PAL); Total  $E_{Ni}$  86% (AL)→94% (PAL)

- ◆ Under pressure condition and longer retention, more Fe/Al precipitate:

$C_{Fe}$  1~2g/L (AL) → 0.75g/L (PAL);  $C_{Al}$  6.5g/L (AL)→0.6g/L (PAL)

Less limestone consumption and less Ni/Co losses in Fe/Al removal

Leaching stage		HPAL-AL	HPAL-PAL	PAL-PAL
Solution/(g/L)	Fe	1.18	0.68	0.75
	Al	6.53	0.63	1.44
Total extraction /%	Ni	<b>86.80</b>	<b>94.10</b>	<b>90.57</b>
SAP — Extraction/%	Ni	<b>56.06</b>	<b>87.34</b>	<b>78.63</b>

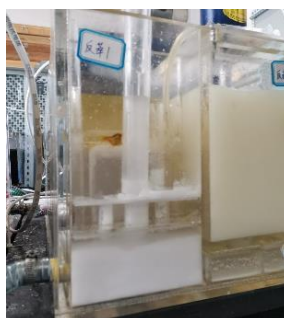
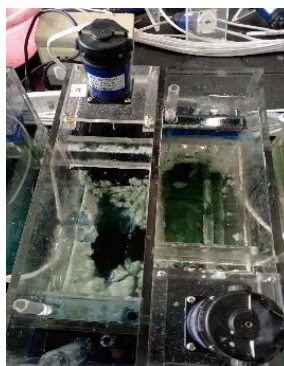
\*LIM / SAP = 100 : 25

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## 3. MHP Refining

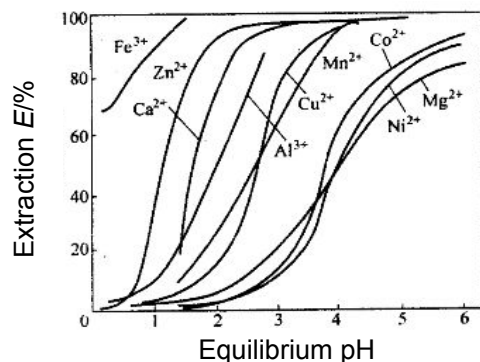
### Disadvantages of current MHP Refining Process

- Large amount Fe/Al residue results in large Ni/Co losses
- $CaSO_4$  crystals scaling
  - CaO to remove Fe/Al.
  - $Ca^{2+}$  saturated.
  - $CaSO_4$  crystals during P204 scrubbing and stripping.
  - $CaSO_4$  scaling on the wall of tank, pipes, impellers, etc..
- Complex SX combination to separate Ni, Co and Mg
  - Ni, Co and Mg separation with C272 and P507, respectively



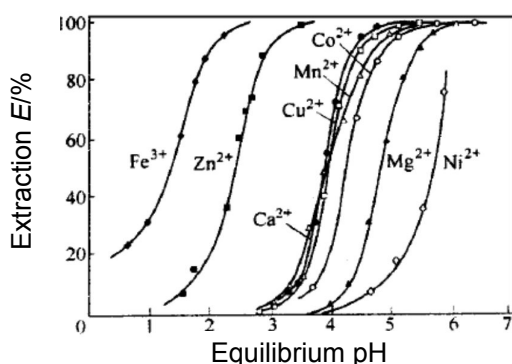
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#### SX isotherm



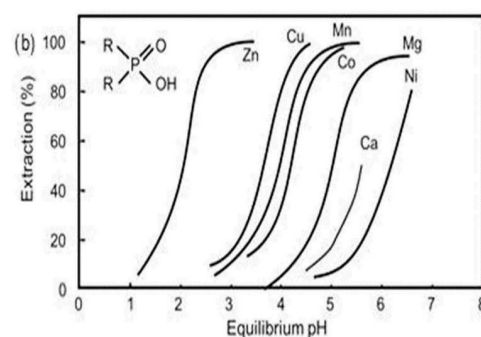
##### □ P204 (D2EHPA)

- Fe<sup>3+</sup> > Zn<sup>2+</sup> > Ca<sup>2+</sup> > Cu<sup>2+</sup> > Mn<sup>2+</sup> > Co<sup>2+</sup> > Mg<sup>2+</sup> > Ni<sup>2+</sup>
- P204: Cu, Zn, Ca, Mn removal



##### □ P507 (PC88A)

- Fe<sup>3+</sup> > Zn<sup>2+</sup> > Ca<sup>2+</sup> ~ Cu<sup>2+</sup> ~ Mn<sup>2+</sup> > Co<sup>2+</sup> > Mg<sup>2+</sup> > Ni<sup>2+</sup>
- P507: Ni, Co, Mg separation



##### □ C272

- Fe<sup>3+</sup> > Zn<sup>2+</sup> > Cu<sup>2+</sup> > Co<sup>2+</sup> > Mg<sup>2+</sup> > Ca<sup>2+</sup> > Ni<sup>2+</sup>
- C272: Ni / Co separation (high efficiency)

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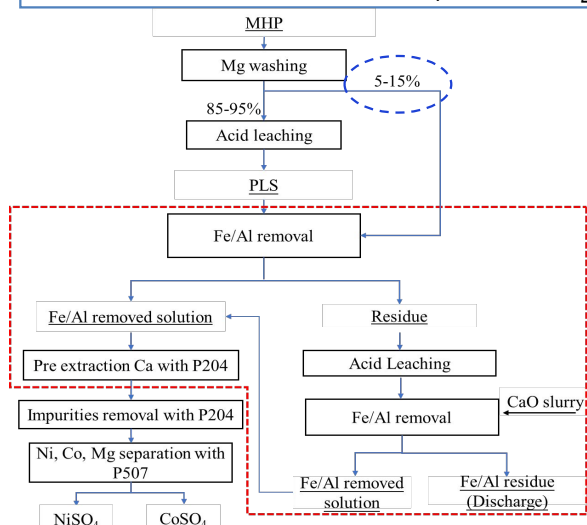
#### MHP Composition (Ramu)

Element	Ca	Co	Ni	Cr	Cu	Cd	Fe
Content/%	0.15	3.92	40.85	0.0193	0.10	<0.001	0.076
Element	Li	Mg	Mn	Si	Pb	P	Al
Content/%	<0.001	1.46	5.25	0.14	0.18	0.063	0.24
Element	Ag	Hg	Na	Ti	Zn		
Content/%	<0.001	0.12	0.34	0.014	0.73		

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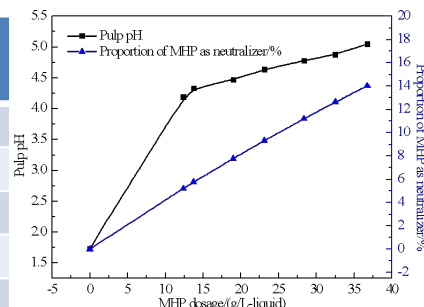
### MHP used to remove Fe/Al/Si

- 5~15% MHP is used in neutralization to remove Fe/Al/Si.
- Consume remaining acid.
- 90% CaO consumption is reduced. Thus, the  $\text{CaSO}_4$  crystallization on scaling is reduced. Meanwhile, Fe/Al residue amount is reduced (less  $\text{CaSO}_4$ ), and Ni&Co losses are reduced.



Results

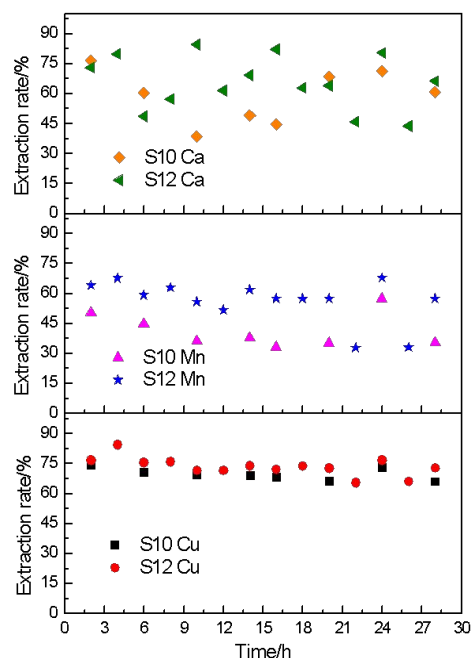
% MHP addition	5.0	11.4	14.7
Final pH	4.19	4.98	5.05
Fe/Al removed solution (g/L)	Fe	<0.001	<0.001
	Al	0.099	0.058
	Cr	0.009	<0.001
	Si	/	/



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### Pre extraction Ca and purification (Cu/Mn/Zn removal) with P204

- Pre extraction Ca with P204.
- 50% Ca is removed.



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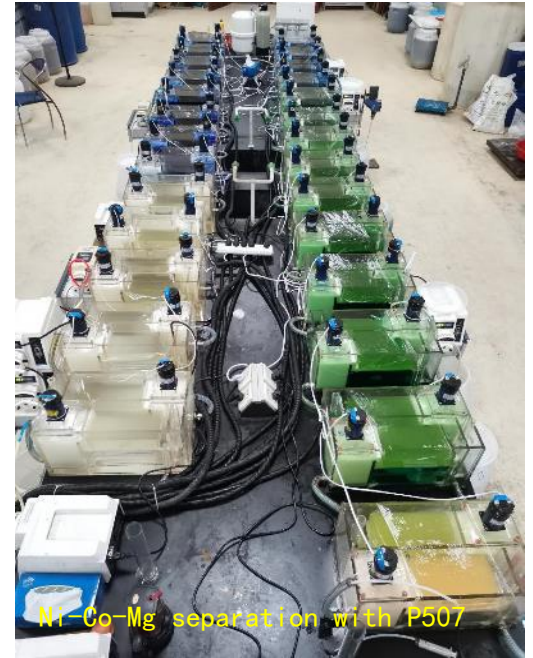


#### Ni/Co/Mg separation in one SX train

- 6 stages Na and Ni saponification – 8 stages Ni extraction – 10 stages Mg scrubbing – 4 stages Co stripping – 2 stages acid scrubbing.
- Ni in raffinate. Separate Mg by scrubbing. Co by stripping.

Product	NiSO <sub>4</sub> ·6H <sub>2</sub> O	CoSO <sub>4</sub> ·7H <sub>2</sub> O
Ca	5.00	5.00
Co	5.00	
Ni		5.00
Cl	50.00	50.00
Cr	5.00	5.00
Cr <sup>6+</sup>	5.00	5.00
Cu	2.00	3.00
Cd	2.00	3.00
Fe	4.00	10.00
K	50.00	50.00
Mg	25.00	25.00
Mn	2.00	3.00
Si	50.00	50.00
Sn	5.00	5.00
Pb	2.00	2.00
Al	30.00	30.00
Mo	10.00	10.00
As	2.00	2.00
Hg	2.00	2.00
Na	50.00	50.00
Zn	2.00	3.00
Minimum Content [w%]		
Ni		22
Co		20.5

Battery grade products



Ni-Co-Mg separation with P507

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#### ◆ Reduction smelting — crude nickel anode electrolysis

##### Hydro-process problems:

- SX process: large acid and alkali consumption, large  $\text{MgSO}_4$  open circuit, large amount of waste water, large amount of hazardous wastes
- Mg removal by fluoride: superfluous  $\text{F}^-$ ;  $\text{F}^-$  has negative impact on Ni electrolysis



Impurities removal by  
pyrometallurgy process

Reduction smelting — crude nickel anode electrolysis —  
anode liquid purification process

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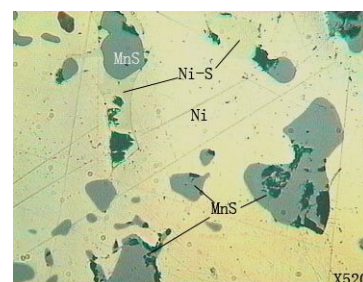
### ◆ Reduction smelting — crude nickel anode electrolysis

Test No.	Metal					
	Ni	Co	Mn	Fe	Cu	Zn
1	85.5	4.03	4.2	1.08	0.10	0.31
2	83.4	3.87	4.50	2.13	0.012	0.006
3	84.2	3.92	4.35	2.29	0.012	0.15
4	77.0	3.20	6.10	1.97	0.012	0.006
5	82.8	4.05	4.54	1.77	0.011	0.001
6	85.6	4.08	4.38	1.84	0.011	0.010
7	84.4	4.05	4.22	1.92	0.012	0.025



Crude nickel buttons

- Ni/Co/Cu mainly enter to metal. Crude nickel contains 80-85% nickel and 4% cobalt.
- Almost all CaO, MgO, Al<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub> enter into slag.
- 85~97% zinc enters into dust. Zn is removed.
- 20% Mn enters into metal and 80% enters into slag.



### ◆ Reduction smelting — crude nickel anode electrolysis

Electrolysis test results

Test No.	Anode current efficiency/%	Cathode current efficiency/%
1	95.8	98.2
2	94.7	99.3
3	94.4	98.9
4	94.7	98.7
5	95.0	98.6
6	95.6	98.9

Nickel cathode composition

Element	Ni+Co	C	S	P	Cu	Pb
Standard*	99.96	0.005	0.001	0.001	0.01	0.001
Test	>99.96	0.0018	0.0004	<0.0001	0.0015	<0.0003
Element	Sn	Sb	Bi	Si	Mn	Mg
Standard*	0.0003	0.0003	0.0003	0.002	-	0.001
Test	<0.0002	0.0002	<0.0005	<0.001	0.0001	<0.001
Element	Zn	Cd	Fe	Al	As	
Standard*	0.0015	0.0003	0.01	-	0.0008	
Test	0.0008	0.0001	0.0021	<0.001	<0.0008	

Standard\*: GB/T 6516-2010



- GB/T 6516-2010 electrolytic nickel standard
- Grade: Ni9996

- ◆ **Inverse leaching (IL) process is very flexible to treat LIM and SAP (Or transitional laterite ore)**
  - Ni extraction ~ 95%, at least 10% higher than ATL.
- ◆ **Two-stage pressure leaching (HPAL — PAL) process is very efficient to treat LIM and SAP**
  - Ni extraction increases greatly. SAP  $E_{Ni}$  50% (AL) → 95% (PAL);
  - PLS:  $C_{Fe}$  1~2g/L (AL) → 0.75g/L (PAL);  $C_{Al}$  6.5g/L (AL) → 0.6g/L (PAL);
  - Less limestone consumption and less Ni/Co losses in Fe/Al removal.

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- ◆ **MHP refining process -- Dissolving and SX-purification -- High pure Ni/Co - sulfates with battery grade**
  - MHP is used in neutralization, to reduce CaO consumption, thus residues and Ni & Co losses could be reduced;
  - Reduction of  $CaSO_4$  crystals during impurities removal with P204 -SX;
  - Ni/Co/Mg separation with P507 in one SX - train;
  - Continuous SX purification and separation flow-sheet.
- ◆ **Reduction smelting — crude nickel anode electrolysis process**
  - High recovery: Ni >97%, Co > 90%;
  - Easy removal of Ca, Mg, Al, Si, Mn and Zn (into slag / dust);
  - Suitable for low grade MHP (low cost), due to low acid and alkali consumption;
  - Environment friendly (much less wastes).

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# Thank you!

## Contact

Email: [jiangkx@bgrimm.com](mailto:jiangkx@bgrimm.com)

Mobile: +86-13601177027

Wechat: KAIXI\_JIANG

